## LETTER TO THE EDITORS

## SOME NOTES ON FORMULATION OF THE PROBLEM OF GAS FLOW IN A CIRCULAR TUBE

STEADY-STATE heat transfer of gas long tube flow at small Mach numbers ( $M \ll 1$ ) and without considering the gravity is described by means of the boundary-layer type equations (1)-(3)

$$\frac{\partial \rho u}{\partial x} + \frac{1}{r} \frac{\partial \rho v r}{\partial r} = 0 \tag{1}$$

$$\rho u \frac{\partial u}{\partial x} + \rho v \frac{\partial u}{\partial r} = -\frac{\mathrm{d}p}{\mathrm{d}x} + \frac{1}{r} \frac{\partial}{\partial r} \left( r \mu \frac{\partial u}{\partial r} \right)$$
(2)

$$\rho u \frac{\partial H}{\partial x} + \rho v \frac{\partial H}{\partial r} = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{k}{C_p} \frac{\partial H}{\partial r} \right)$$
(3)

while initial and boundary conditions must be written in the following form

$$H(0,r) = H_0(r), \quad u(0,r) = u_0(r), \quad p(0) = p_0$$
 (4)

$$\frac{\partial H}{\partial r}(x,0) = 0, \quad \frac{\partial u}{\partial r}(x,0) = 0, \quad v(x,0) = 0$$
$$-\frac{k}{C_p} \frac{\partial H}{\partial r}(x,r_w) = q_w(x) \text{ or } H(x,r_w) = H_w(x),$$
$$u(x,r_w) = 0, \quad v(x,r_w) = 0.$$
(5)

It is shown in paper [1] that the written conditions are enough for solving equations in the region of  $\Omega$  ( $x \ge 0$ ,  $0 \le r \le r_{w}$ ). However in papers [2, 3] the problem is overdetermined by giving the profile v(0,r) in the starting crosssection. Furthermore, in paper [2] the starting cross-section profile  $\rho(0,r)$  is given which cannot be taken arbitrary, since the pressure corresponding to density and enthalpy must be constant in the cross-section.

It ought to be explained why exactly the giving of v(0,r) is superfluous. As the solution of our problem (1)-(5) at x = 0 cannot be conjugated with an arbitrary flow from the left-hand side, the surface x = 0 is to be considered the discontinuity surface. Presenting the equations (1)-(3) in the conservation form

$$\frac{\partial \rho ur}{\partial x} + \frac{\partial \rho vr}{\partial r} = 0 \qquad (1')$$

$$\frac{\partial(p+\rho u^2)r}{\partial x}+\frac{\partial\rho uvr}{\partial r}=\frac{\partial}{\partial r}\left(r\mu\frac{\partial\mu}{\partial r}\right)$$
(2')

$$\frac{\partial \rho u H r}{\partial x} + \frac{\partial \rho v H r}{\partial r} = \frac{\partial}{\partial r} \left( r \frac{k}{C_n} \frac{\partial H}{\partial r} \right)$$
(3')

we can derive from them the conservation conditions which must be true on the discontinuity surface x = 0 [4]

$$[\rho u] = 0, \quad [p + \rho u^2] = 0, \quad [p u H] = 0. \tag{6}$$

Consequently, while crossing the surface x = 0 the parameter values u, H and p are conserved and only the radial velocity v may have discontinuity.

Since in the problem under consideration  $(\partial p/\partial r) = 0$ and  $(dp/dx) \sim M^2$ , then  $\rho$ ,  $\mu$ , k,  $C_p$  can be assumed to be prescribed temperature functions only. In this case the system of equations (1)-(3) with boundary conditions (5) permits stretching at  $q_w = \text{const}$  (or  $H_w = \text{const}$ ):

$$x' = \alpha x, \quad r' = r, \quad u' = \alpha u, \quad v' = v, \quad H' = H,$$
  
$$\left(\frac{\mathrm{d}p}{\mathrm{d}x}\right)' = \alpha \left(\frac{\mathrm{d}p}{\mathrm{d}x}\right) \quad (7)$$

which allows nondimensional parameters to be introduced, so that the Reynolds number will not enter into the equations and boundary conditions [1]. That means that the obtained solution can be re-evaluated for the flow with similar initial axial velocity profile by means of simple stretching of the x-coordinate.

We point out that equation (1d) included in the initial system of equations in paper [2] is not independent. It may be derived by radial integration of the continuity equation using boundary conditions for v.

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