LETTER TO THE EDITORS

SOME NOTES ON FORMULATION OF THE PROBLEM OF GAS FLOW IN A CIRCULAR TUBE

STEADY-STATE heat transfer of gas long tube flow at small Mach numbers $(M \ll 1)$ and without considering the gravity is described by means of the boundary-layer type equations (1) - (3)

$$
\frac{\partial \rho u}{\partial x} + \frac{1}{r} \frac{\partial \rho v r}{\partial r} = 0 \tag{1}
$$

$$
\rho u \frac{\partial u}{\partial x} + \rho v \frac{\partial u}{\partial r} = -\frac{dp}{dx} + \frac{1}{r} \frac{\partial}{\partial r} \left(r \mu \frac{\partial u}{\partial r} \right) \tag{2}
$$

$$
\rho u \frac{\partial H}{\partial x} + \rho v \frac{\partial H}{\partial r} = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{k}{C_p} \frac{\partial H}{\partial r} \right) \tag{3}
$$

while initial and boundary conditions must be written in the following form

$$
H(0,r) = H_0(r), \quad u(0,r) = u_0(r), \quad p(0) = p_0 \tag{4}
$$

$$
\frac{\partial H}{\partial r}(x,0) = 0, \quad \frac{\partial u}{\partial r}(x,0) = 0, \quad v(x,0) = 0
$$

$$
-\frac{k}{C_p} \frac{\partial H}{\partial r}(x,r_w) = q_w(x) \text{ or } H(x,r_w) = H_w(x),
$$

$$
u(x,r_w) = 0, \quad v(x,r_w) = 0.
$$
(5)

It is shown in paper [I] that the written conditions are enough for solving equations in the region of Ω (x ≥ 0 , $0 \le r \le r_{\rm w}$). However in papers [2, 3] the problem is overdetermined by giving the profile $v(0,r)$ in the starting crosssection. Furthermore, in paper [2] the starting cross-section profile $\rho(0,r)$ is given which cannot be taken arbitrary, since the pressure corresponding to density and enthalpy must be constant in the cross-section.

It ought to be explained why exactly the giving of $v(0,r)$ is superfluous. As the solution of our problem (1) - (5) at $x = 0$ cannot be conjugated with an arbitrary flow from the left-hand side, the surface $x = 0$ is to be considered the discontinuity surface. Presenting the equations $(1)+(3)$ in the conservation form

$$
\frac{\partial \rho u r}{\partial x} + \frac{\partial \rho v r}{\partial r} = 0 \tag{1'}
$$

$$
\frac{\partial (p + \rho u^2)r}{\partial x} + \frac{\partial \rho uvr}{\partial r} = \frac{\partial}{\partial r} \left(r\mu \frac{\partial \mu}{\partial r} \right) \tag{2}
$$

$$
\frac{\partial \rho u Hr}{\partial x} + \frac{\partial \rho v Hr}{\partial r} = \frac{\partial}{\partial r} \left(r \frac{k}{C_n} \frac{\partial H}{\partial r} \right) \tag{3'}
$$

we can derive from them the conservation conditions which must be true on the discontinuity surface $x = 0$ [4]

$$
[\rho u] = 0, \quad [p + \rho u^2] = 0, \quad [puH] = 0. \tag{6}
$$

Consequently, while crossing the surface $x = 0$ the parameter values u , H and p are conserved and only the radial velocity u may have discontinuity.

Since in the problem under consideration $(\partial p/\partial r) = 0$ and $(dp/dx) \sim M^2$, then ρ , μ , k , C_p can be assumed to be prescribed temperature functions only. In this case the system of equations (1) - (3) with boundary conditions (5) permits stretching at $q_w = \text{const}$ (or $H_w = \text{const}$):

$$
x' = \alpha x, \quad r' = r, \quad u' = \alpha u, \quad v' = v, \quad H' = H,
$$

$$
\left(\frac{dp}{dx}\right)' = \alpha \left(\frac{dp}{dx}\right) \tag{7}
$$

which allows nondimensional parameters to be introduced, so that the Reynolds number will not enter into the equations and boundary conditions [I]. That means that the obtained solution can be re-evaluated for the flow with similar initial axial velocity profile by means of simple stretching **of** the .x-coordinate.

We point out that equation (1d) included in the initial system of equations in paper [Z] is not independent. ft may be derived by radial integration of the continuity equation using boundary conditions for v.

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